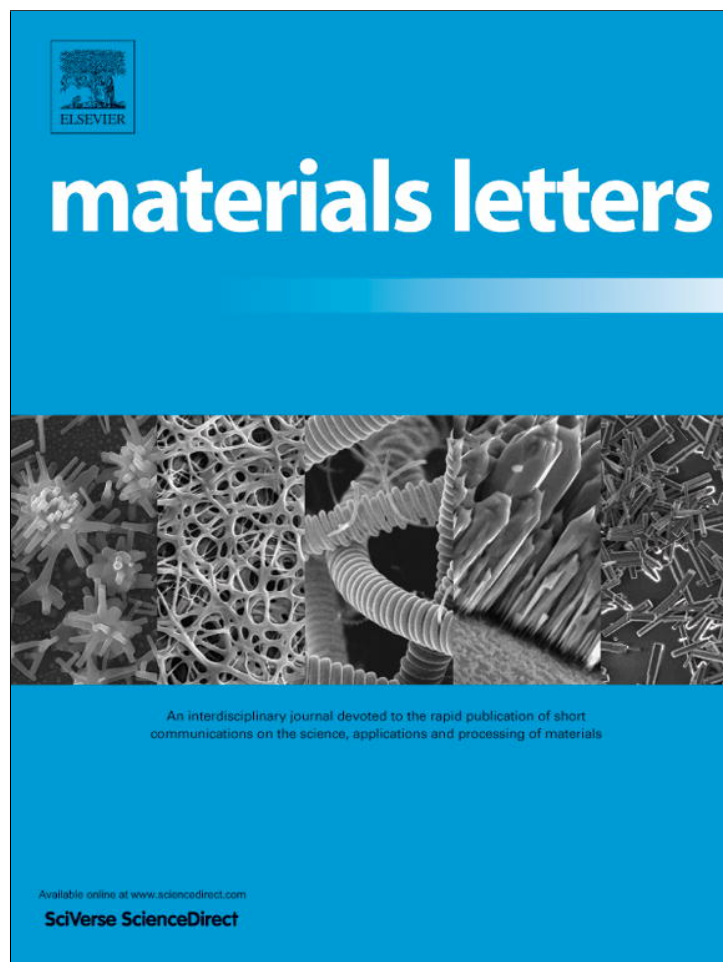


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Phase transformations in the severely plastically deformed Zr–Nb alloys

B.B. Straumal^{a,b,*}, A.S. Gornakova^a, A.A. Mazilkin^{a,b}, O.B. Fabrichnaya^c, M.J. Kriegel^c, B. Baretzky^b, J.-Z. Jiang^d, S.V. Dobatkin^e

^a Institute of Solid State Physics RAS, 142432 Chernogolovka, Russia

^b Karlsruher Institut für Technologie, Institut für Nanotechnologie, Hermann-von-Helmholtz-Platz 1, 76344 Eggenstein-Leopoldshafen, Germany

^c TU Bergakademie Freiberg, Institut für Werkstoffwissenschaft, 09599 Freiberg, Germany

^d Department of Materials Science and Engineering, Zhejiang University, 310027 Hangzhou, China

^e Institute of Metallurgy and Materials Science RAS, 117991 Moscow, Russia

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ABSTRACT

Zr–Nb alloys play the important role in the energy production of being the main material for the cladding of nuclear fuel in the nuclear power plants. Severe plastic deformation by high-pressure torsion (HPT) leads to the strong grain refinement in Zr–Nb alloys. HPT leads also to formation of the high-pressure ω Zr phase. It remains quenched at the ambient pressure and disappears by heating only above 400 °C. The diffusion-controlled α Zr + β Nb \rightarrow α Zr + β Zr \rightarrow β Zr transformations are observed only in the as-cast alloy Zr–2.5 mass% Nb. Transformation α Zr \leftrightarrow β Zr in as-cast alloy Zr–8 mass% Nb occurs as martensitic. Phase transformations occurring in alloys of both compositions after HPT on heating are martensitic. The effective temperature during HPT has been determined as $T_{\text{eff}} = 700$ °C at 5 GPa.

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1. Introduction

Zr–Nb alloys play the important role in the energy production of being the main material for the cladding of nuclear fuel in the nuclear power plants [1,2]. Severe plastic deformation (SPD) permits to obtain the extremely fine-grained structure in Zr and Zr alloys [3–5 and references therein]. They contain also the high pressure ω -phase which remains quenched after the release of high pressure. If one compares the phases in alloys before and after SPD with an equilibrium phase diagram, one can estimate the effective temperature during SPD treatment [6]. The investigation of peculiarities of phase transformations in the SPD-treated Zr–Nb alloys was the goal of this work.

2. Experimental

Two Zr–Nb alloys with 2.5 and 8 wt.% Nb were melted in a vacuum with high purity components (4 N Zr and 4 N Nb). The cast disks of 0.7 mm thick were deformed by high-pressure torsion (HPT) at 5 GPa (5 torsions, 1 rotation-per-minute). X-ray diffraction (XRD) data were obtained on a Siemens diffractometer (Co K_{α} radiation). Grain size was estimated by XRD line broadening using the Scherer formula [7]. Both the as-cast and fine-grained HPT-samples were studied by differential scanning calorimetry (DSC) in the temperature range of 100–900 °C using the NETZSCH Pegasus 404C calorimeter in

the dry argon atmosphere, in Al_2O_3 crucibles and at the cooling and heating rates of 20 K/min. Thermodynamic calculations were performed using the thermodynamic data of Guillermet [8] where solid solutions with bcc and hcp (α Zr) structures as well as liquid solution were described by using a substitutional model. The bcc phase is described as single phase which forms miscibility gap β Zr + β Nb in the composition range from 8 to 81 wt.% Zr and temperatures from 620 up to 976 °C. Thermo-calc software [9] was used to calculate equilibrium phase diagrams and diffusionless transformation α Zr \leftrightarrow β Zr.

3. Results and discussion

The grain size in both as-cast alloys was about 500–800 μm [10]. HPT drastically refined the grains. Grain size after HPT was only about 20 nm. XRD-spectra of as-cast alloys (Fig. 1a) demonstrate that they contain mainly α Zr with hexagonal closely-packed (hcp) lattice. The Nb-rich body-centered cubic (bcc) phase (β Nb in Fig. 2) is absent. Small amount of β Zr is present in the as-cast alloys. Zr-rich β Zr has a body-centered cubic lattice and is isomorphous to the Nb-rich phase (β Nb). The calculated phase diagram (Fig. 2a) reproduces experimental data [11] very well. Below the temperature of a monotectoid transformation $T_{\text{mon}} = 620$ °C the stable assemblage is β Nb + α Zr according to the Zr–Nb phase diagram (Fig. 2a). Above monotectoid reaction at composition $\text{Zr} > 81$ mass% β Zr is in equilibrium with α Zr phase which transforms into β Zr single phase with temperature increase. For compositions with Zr content between 8 and 81 wt.% and temperatures between monotectoid reaction and critical point $T_c = 976$ °C there is a two-phase area β Nb + β Zr

* Corresponding author at: Institute of Solid State Physics RAS, 142432 Chernogolovka, Russia. Tel./fax: +7 499 2382326.

E-mail address: straumal@issp.ac.ru (B.B. Straumal).

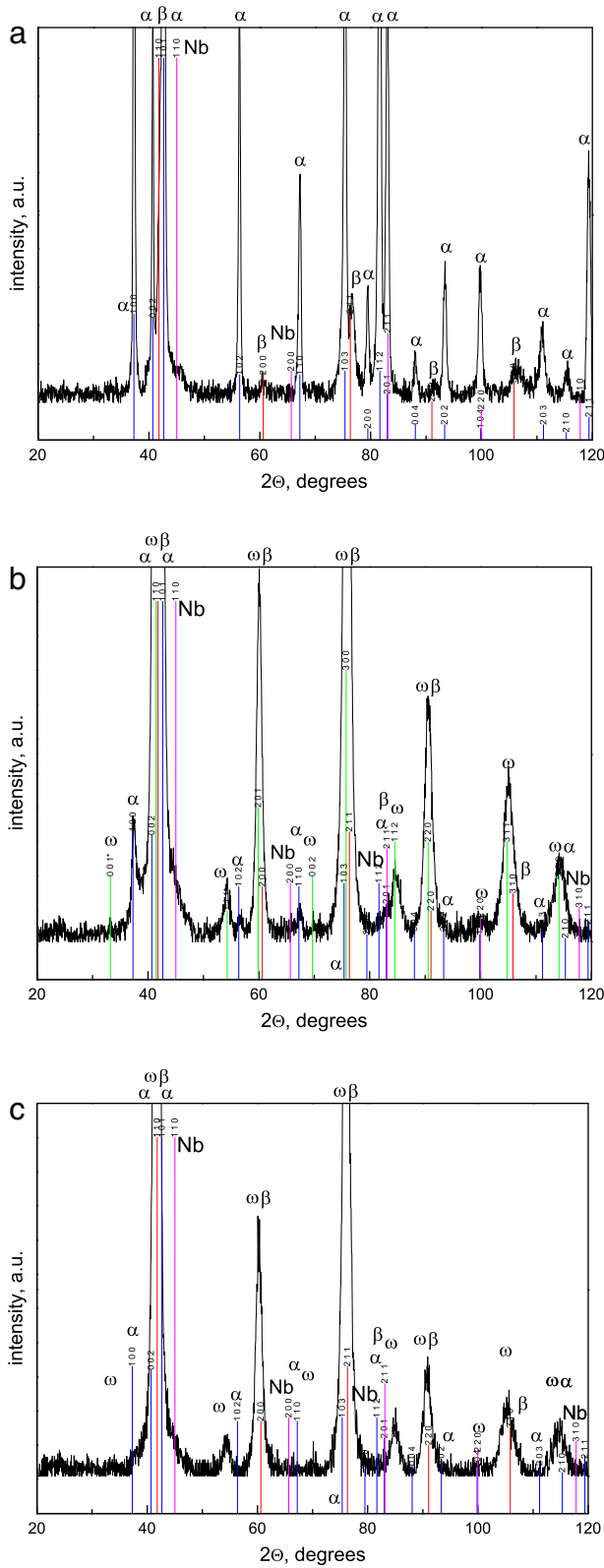


Fig. 1. XRD curves for the (a) as-cast CG Zr-2.5 wt.% Nb alloy, (b) UFG Zr-2.5 wt.% Nb alloy after HPT and (c) UFG Zr-8 wt.% Nb alloy after HPT.

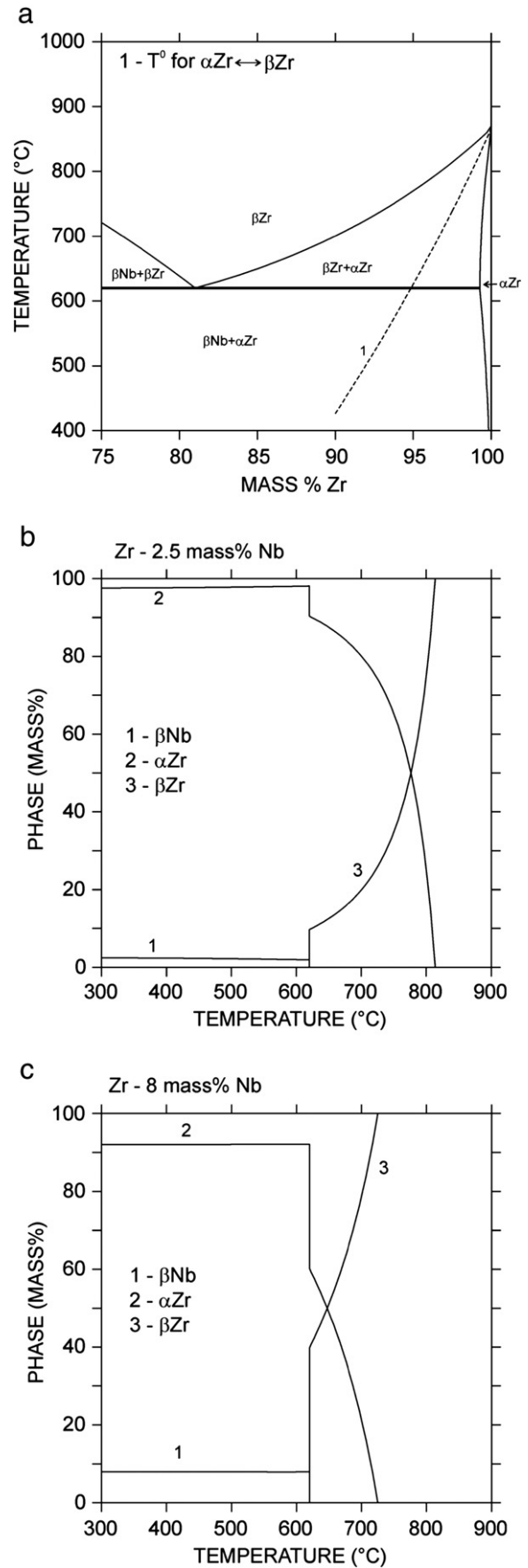


Fig. 2. (a) The part of the Zr-Nb phase diagram and temperature dependence of the equilibrium amount of βNb, αZr and βZr phases forming the (b) Zr-2.5 wt.% Nb and (c) Zr-8 wt.% Nb alloys calculated using the THERMO-CALC program. Dashed line in (a) shows the martensitic αZr → βZr transformation.

(Fig. 2a). After HPT both fine-grained Zr–Nb alloys contain mainly the ω Zr phase (Fig. 1b,c) with hexagonal C32 structure [12]. At the diffraction angle $2\theta = 54^\circ$ the peak of a ω Zr (C32) phase is clearly visible without overlapping with peaks of other phases. α Zr (hcp-phase) almost disappeared after HPT. The Nb-rich bcc phase (β Nb) is absent both after and before HPT. All diffraction peaks of the β Zr phase are very close to the peaks of ω Zr phase. Nevertheless, the positions of peaks at $2\theta = 60^\circ, 76^\circ, 91^\circ$ and 105° for the Zr–2.5 wt.% Nb alloy after HPT (Fig. 1b) almost perfectly coincide with the tabulated values for 201, 300, 220 and 311 peaks for the ω Zr phase. In the Zr–2.5 wt.% Nb alloy the same diffraction peaks are shifted to the right and are positioned between the respective tabulated values for the ω Zr and β Zr phases. In other words, the amount of β Zr phase after HPT is much higher in the Zr–2.5 wt.% Nb alloy than in the Zr–8 wt.% Nb one.

In Fig. 3 the temperature dependences of heat flow (DSC curves) and its time derivative DDSC are shown for the as-cast and HPT-treated Zr–Nb alloys. In the as-cast Zr–2.5 wt.% Nb alloy (Fig. 3a) three heat effects are clearly visible. The onset at 505°C can be due to the transformation of retained β Zr which was found in as-cast alloys (Fig. 1a) into equilibrium assemblage β Nb + α Zr. The second one is due to monotectoid reaction α Zr + β Nb \rightarrow β Zr (onset at 623.1°C) and the third one is due to change of the α Zr + β Zr two-phase area into single β Zr phase around 746°C (onset) showing deep minimum at 815°C . These temperatures (623 and 815°C) agree with the respective ones in the equilibrium Zr–Nb phase diagram (Fig. 2). During cooling the transformation of β Zr into β Zr + α Zr assemblage was observed at slightly lower temperature ($\sim 790^\circ\text{C}$). These results agree with the data of Stewart et al. [13], who showed that Zr alloys with 3.05 wt.% Nb transforms into α Zr + β Zr and β Zr single phase by nucleation and growth mechanism at cooling rates below 10 K/s. The DSC curve for the as-cast Zr–8 wt.% Nb alloy looks different (Fig. 3b). The non-equilibrium phase β Zr found in as-cast Zr–8 wt.% Nb alloy transforms into α Zr phase at 445°C , which transforms into β Zr at 511°C by diffusionless mechanism. This is in agreement with calculated α Zr \rightarrow β Zr

transformation shown by a dashed line in Fig. 2a. At further heating martensite β Zr continuously transforms into equilibrium assemblage α Zr + β Zr which finally transforms into stable β Zr at 730°C corresponding to deep minimum at DSC curve. The curves for the HPT-treated samples are presented in Fig. 3c–d. Reaction with a very pronounced heat effect starts at 492.2°C in the Zr–2.5 wt.% Nb alloy and at 459.3°C in the Zr–8 wt.% Nb alloy. Heat effects at these temperatures were not observed if the HPT-treated samples were heated again after the first DSC-run. Therefore, they can be attributed with transformation of metastable ω Zr into α Zr phase. These results are also in agreement with the temperature of ω Zr formation during fast cooling at 400 – 450°C [13]. The difference between DCS curves in the first and second runs are definitely influenced also by the (inevitable) grain growth in the HPT-treated alloy [14,15]. The heat effect of the recrystallization of nanograined SPD-treated alloys during diffusion anneals has been analyzed recently in Ref. [14]. The grain growth heat releases during first DSC run and does not appear during the second one. It has to be underlined that the amount of ω Zr was lower in the Zr–8 wt.% Nb alloy and that it transformed to α Zr phase at lower temperature. The second feature in alloy Zr–2.5 wt.% Nb at 568.4°C can be explained by the transformation of metastable β Zr found in HPT treated alloy into α Zr phase. The second heat effect for Zr–8 wt.% Nb alloy at 519°C can be explained by diffusionless transformation of α Zr to β Zr which is in agreement with calculated temperature α Zr \rightarrow β Zr (503°C). It should be mentioned that all transformations at temperatures below 620°C occur by diffusionless mechanism. It is known that the $\alpha \leftrightarrow \beta$ transition in Zr and Ti alloys can proceed as diffusionless martensitic one [16,17]. The martensite α Zr in Zr–2.5 wt.% Nb alloy at temperatures above monotectoid reaction was continuously transforming into equilibrium α Zr + β Zr assemblage up to formation of single β Zr phase. This transformation corresponds to the deep minima in DSC curves at 750°C . Martensite β Zr in the Zr–8 wt.% Nb alloy was continuously transforming into equilibrium α Zr + β Zr assemblage up to formation of β Zr at 710°C . The grain size effect on the presence or absence of martensitic

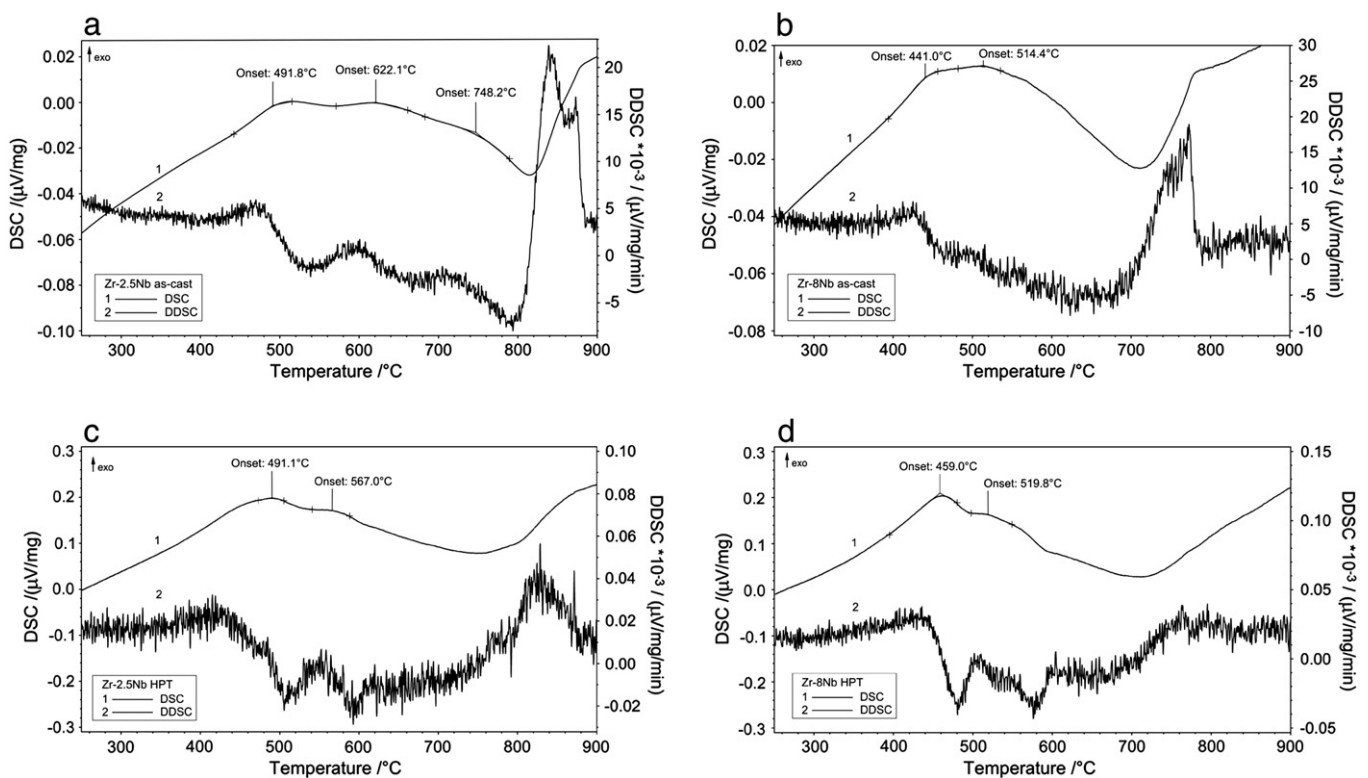


Fig. 3. The temperature dependences of heat flow DSC (upper curves) and its time derivative DDSC (lower curves) for (a) as-cast Zr–2.5 wt.% Nb alloy, (b) as-cast Zr–8 wt.% Nb alloy, (c) UFG Zr–2.5 wt.% Nb alloy after HPT and (d) UFG Zr–8 wt.% Nb alloy after HPT.

transformation has been observed in precipitates in Zr–1 wt.% Nb alloy [17]. Therefore, we can suppose that the clear change from diffusional to martensitic transformations in the HPT-treated Zr–Nb alloys in comparison with as-cast alloys could be due to the SPD-driven grain refinement.

Usually, the high pressure decreases the diffusivity and grain boundary mobility [18,19]. However, the atom movements caused by strong external forces can drive both accelerated diffusion and phase transformations in the material [10]. Following the idea proposed for the materials under severe irradiation [20], we suppose that the forced mixing emulates the increase of entropy and changes the thermodynamic potentials in the alloy. As a result, the phases forming during SPD do not correspond to the equilibrium at the treatment temperature. One can find them in an equilibrium phase diagram at a higher temperature called effective temperature T_{eff} . The HPT-treatment in our work at 5 GPa allowed the formation of the ω Zr high-pressure allotrope. The ω Zr phase became stable at room temperature above 3.4 GPa [21] and remained in our samples also at ambient pressure after SPD-treatment. Such phenomenon has been observed both in Zr- and Ti-based alloys but not in Hf [3–5 and references therein]. Therefore, in order to determine T_{eff} one has to use the equilibrium phase diagram at high pressures. The mixture of ω Zr and β Zr phases in the absence of α Zr is present at 5 GPa in the narrow interval between 680 and 720 °C [22]. Therefore, in our case $T_{\text{eff}} = 700$ °C.

4. Conclusions

(1) Severe plastic deformation by HPT leads to the strong grain refinement in Zr–Nb alloys; (2) the high-pressure ω Zr phase appears during HPT and remains quenched in both studied alloys at the ambient pressure; (3) ω Zr phase disappears by heating only between 400 and 500 °C; (4) the α Zr + β Nb \leftrightarrow α Zr + β Zr \leftrightarrow β Zr transformations are diffusion-controlled in the as-cast alloy Zr–2.5 mass% Nb while transformation α Zr \leftrightarrow β Zr in the as-cast alloy Zr–8 mass% Nb is martensitic. The transformations of ω Zr in both ultra-fine-grained alloys after

HPT-treatment occur by diffusionless mechanism. The effective temperature during HPT has been determined as $T_{\text{eff}} = 700$ °C.

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References

- [1] Beskorovainyi NM, Kalin BA, Platonov PA, Chernov II. Structural materials for nuclear reactors. Moscow: Energoatomisdat; 1995 (in Russian).
- [2] Zuev LB, Semukhin BS, Zavodchikov SY. Mater Lett 2005;57:1015–20.
- [3] Zhilyaev AP, Sabirov I, González-Doncela G, Molina-Aldareguía J, Srinivasarao B, Pérez-Prado MT. Mater Sci Eng A 2011;528:3496–505.
- [4] Edalati K, Matsubara E, Horita Z. Metall Mater Trans A 2009;40:2079–86.
- [5] Edalati K, Horita Z, Mine Y. Mater Sci Eng A 2010;527:2136–41.
- [6] Straumal BB, Mazilkin AA, Baretzky B, Rabkin E, Valiev RZ. Mater Trans 2012;53:63–71.
- [7] Ungar T, Borbely A. Appl Phys Lett 1996;69:3173–5.
- [8] Guillermet AF. Z Metallkd 1991;82:478–87.
- [9] Andresson J-O, Helander T, Höglund L, Shi P, Sundman B. Calphad 2002;26:273–312.
- [10] Straumal BB, Gornakova AS, Kucheev YO, Baretzky B, Nekrasov AN. J Mater Eng Perform 2012;21, doi:10.1007/s11665-012-0158-7.
- [11] Massalski TB, editor. Binary alloy phase diagrams. 2nd ed. Materials Park, OH: ASM International; 1990.
- [12] Sikka SK, Vohra YK, Chidambaram R. Prog Mater Sci 1982;27:245–310.
- [13] Stewart D, Hatt BA, Roberts JA. Br J Appl Phys 1965;16:1081–8.
- [14] Amouyal Y, Divinski SV, Klinger L, Rabkin E. Acta Mater 2008;56:5500–13.
- [15] Straumal BB, Kogtenkova OA, Protasova SG, Zięba P, Czepe T, Baretzky B, et al. J Mater Sci 2011;46:4243–7.
- [16] Davis R, Flower HM, West DRF. J Mater Sci 1975;14:712–22.
- [17] Neogy S, Krishna KVM, Srivastava D, Dey GK. Philos Mag 2011;91:4447–64.
- [18] Kedves FJ, Erdélyi G. Def Diff Forum 1989;66–69:175–88.
- [19] Molodov DA, Straumal BB, Shvindlerman LS. Scr Metall 1984;18:207–11.
- [20] Martin G. Phys Rev B 1984;30:1424–36.
- [21] Zhang J, Zhao Y, Pantea C, Qian J, Rigg P, Hixson R, et al. J Phys Chem Solids 2005;66:1213–9.
- [22] Zhang J, Zhao Y, Rigg PA, Hixson RS, Gray III GT. J Phys Chem Solids 2007;68:2297–302.